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LIGHTWEIGHT UNDERWATER ACOUSTIC PROJECTOR

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT (1) THOMAS R. HOWARTH, (2) JAMES F. TRESSLER and (3) WALTER L. CARNEY, citizens of the United States of America, employees of the United States Government and residents of (1) Washington, District of Columbia, (2) Alexandria, County of Fairfax, Commonwealth of Virginia and (3) Bloomfield, County of Greene, State of Indiana have invented certain new and useful improvements entitled as set forth above of which the following is a specification:

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5 Nov 2002
DATE OF SIGNATURE



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3 LIGHTWEIGHT UNDERWATER ACOUSTIC PROJECTOR

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5 STATEMENT OF GOVERNMENT INTEREST

6 The invention described herein may be manufactured and used
7 by or for the Government of the United States of America for
8 governmental purposes without the payment of any royalties
9 thereon or therefore.

10

11 BACKGROUND OF THE INVENTION

12 (1) Field Of The Invention

13 This invention relates to acoustic projectors for sonar use
14 and more particularly to a lightweight acoustic projector that
15 can be used by itself or in an array.

16 (2) Description Of The Prior Art

17 Low frequency transducers having resonances below about 10
18 kHz have numerous applications, one of which is as a low
19 frequency sonar projector. This acoustic wavelength
20 corresponding to these frequencies is on the order of the size of
21 naval mines, and thus can hunt for and/or classify them, as well
22 as objects of similar size. Also, wavelengths of this size
23 permit sonar location of buried objects, a task of interest to a
24 wide range of commercial and governmental concerns.
25 Unfortunately, current underwater projectors at these frequencies

1 are large and heavy, and are cumbersome to use on many underwater
2 vehicles.

3 The U.S. Navy is particularly interested in detecting
4 objects in littoral environments for which small, unmanned
5 submersible vehicles are best-suited. Because of the size
6 constraint of the vehicles, it is necessary to keep the
7 dimensions of the associated acoustic projector systems small,
8 particularly along the protrusion dimensions. Acoustically, the
9 desire is for an acoustic source level greater than 180 dB, while
10 geometrically the projector systems need to be thin (less than
11 60-65 mm) for installation onto the sides of underwater vehicles
12 and tow sleds ranging in diameter from 15 cm to over 2.4 meters.
13 Conventional transducer designs used to generate high power sound
14 waves at frequencies under 30 kHz include free-flooded
15 piezoelectric ceramic rings, electromagnetic and hydraulic
16 drivers, tonpils or piston transducers, and flextensional
17 devices. However, because of their large size and weight, these
18 technologies are not easily adaptable for mounting on advanced
19 smaller underwater vehicle platforms.

20 There are also two other potential low frequency acoustic
21 source candidates: 1-3 type piezocomposites and cymbal-based flat
22 panels. Present state-of-the-art 1-3 piezocomposites have a
23 thickness of 25.4 mm and although this meets the dimensional
24 requirements, it also means that their acoustic source level at
25 frequencies below 10 kHz is lower than desired. To form thicker

1 1-3 materials requires extensive electronic matching difficulties
2 and impractical manufacturing and handling requirements. United
3 States Patent No. 6,438,242 to Howarth discloses a cymbal-based
4 flat panel projector that meets the dimensional requirements. In
5 this projector design, miniature flextensional electro-mechanical
6 drivers that are known as 'cymbals' are used to drive a stiff
7 radiating plate. In order to realize optimal acoustic output at
8 low frequencies, an air gap between the radiating plates is
9 required. The typical resonance frequencies for the thin panel
10 projectors is less than 2 kHz. The flat panel design does not
11 allow independent addressing of the projectors. Furthermore, the
12 flat panel imposes an averaging affect on the signal received by
13 each projector.

14

15

SUMMARY OF THE INVENTION

16 Accordingly, an object of the invention is to reduce the
17 cost of active electro-acoustic transducers by use of inherently
18 inexpensive cymbal-type actuators.

19 Another object is to do the foregoing with a transducer that
20 is inherently rugged.

21 Yet another object is to provide an acoustic projector that
22 is small, lightweight, and has low vehicle volume occupation.

23 Still another object is to provide an acoustic projector
24 that allows independent addressing of each projector element.

1 Accordingly, the invention provides a compound electro-
2 acoustic transducer for producing acoustic signals which has a
3 plurality of elements. Each element has a piezoelectric disk
4 with electrically conductive plates fixed on the top and bottom
5 sides of the piezoelectric disk. A stud is joined to an outer
6 face of each plate. Conductors can be joined to each stud. The
7 elements can be assembled on a resilient structure to form an
8 array. Elements can be used in the array or individually
9 accessed.

10

11 BRIEF DESCRIPTION OF THE DRAWINGS

12 These and other features and advantages of the present
13 invention will be better understood in view of the following
14 description of the invention taken together with the drawings
15 wherein:

16 FIG. 1 is a cross-sectional view of a single cymbal driver
17 in accordance with this invention;

18 FIG. 2A is a partially cross-sectional view of a single
19 cymbal driver mounted on a support structure; and

20 FIG. 2B is a partially cross-sectional view of multiple
21 cymbal drivers mounted on a support structure as an array;

22 FIG. 2C is a top view of multiple cymbal drivers mounted as
23 an array;

24 FIG. 3A is a partially cross-sectional view of a single
25 cymbal driver mounted on an alternative support structure;

1 FIG. 3B is a partially cross-sectional view of multiple
2 cymbal drivers mounted on the alternative support structure as an
3 array; and

4 FIG. 3C is a top view of multiple cymbal drivers mounted as
5 an array on the alternative support structure; and

6 FIG. 4 is a top view of an alternate electrical connection
7 structure for the array.

8

9 DESCRIPTION OF THE PREFERRED EMBODIMENT

10 This invention describes a thin, lightweight underwater
11 electroacoustic projector with high acoustic output at
12 frequencies from 0.5 kHz to approaching 1 MHz, with an initial
13 resonance output below 10 kHz. In the design described herein,
14 the preferred frequency band of operation is 2.5 kHz to 100 kHz.
15 The device consists of miniature flextensional electro-mechanical
16 drivers that are known as 'cymbals'. FIG. 1 shows a
17 cross-sectional rendering of the cymbal-type driver 10 used in
18 this device. The active material in each driver 10 is a lead
19 zirconate titanate (PZT) piezoelectric ceramic disk 12 poled in
20 its thickness direction. An electrically conductive structural
21 adhesive 14 is used to mechanically and electrically couple
22 conductive endcaps 16A and 16B to the top and bottom faces of the
23 piezoelectric ceramic disk 12. The endcaps 16A and 16B are
24 shaped such that a shallow air cavity 18 is formed between the
25 cap 16A and 16B and the disk 12 after they are bonded together.

1 Prior to bonding to the disk, threaded studs 20A and 20B are
2 microwelded onto the apex of each of the endcaps 16A and 16B,
3 respectively. For this purpose, each stud 20A and 20B can be
4 provided with bosses 21 to provide a better mounting surface.
5 The ceramic disk 12 and endcaps 16A and 16B can be sealed by
6 applying a water proof coating 22 around the periphery of the
7 assembly.

8 The studs 20A and 20B, in conjunction with the endcaps 16A
9 and 16B, serve as the electrical conduit from the piezoelectric
10 ceramic disk 12 to the electrical lead wires. When an electrical
11 signal is applied to the piezoelectric ceramic disk 12, it either
12 expands or contracts in the radial direction. This expansion and
13 contraction of the piezoelectric ceramic disk 12 causes the dome
14 of the endcaps 16A and 16B to flex. The flexure of the endcaps
15 16A and 16B subsequently produces the low frequency sound waves
16 that are transmitted into the surrounding medium. The magnitude
17 of the acoustic output, its resonance frequency, and hydrostatic
18 pressure tolerance of an individual cymbal element 10 are
19 dependent upon its dimensions, the geometry of the endcaps, and
20 the materials properties of the components.

21 In order to enhance acoustic output, lower the fundamental
22 resonance frequency, and provide for directionality of the
23 generated sound, the individual cymbal elements 10 are
24 incorporated into an array. For incorporating the cymbal
25 elements 10 into an array, the individual elements 10 must be

1 mounted in a way that does not transmit vibrations between the
2 elements, yet acts to hold the elements in a predetermined
3 configuration.

4 FIG. 2A shows one way to electrically interconnect the
5 individual cymbal elements in a mounting 24. In this case, metal
6 ribbon 28A is used to connect one side of all of the cymbal
7 elements 10. The other pole of cymbal element 10 is connected to
8 metal ribbon 28B. Together, this results in a parallel
9 electrical connection of all of the elements. The ribbons 28A
10 and 28B maintain mechanical and electrical contact with the
11 respective studs 20A and 20B via nuts 30 and washers 32. FIG.
12 2B shows a partially cutaway side views of an array of cymbal
13 elements 10 held in the mounting 24. FIG. 2C is a view looking
14 from the top of the array.

15 FIGS. 3A, 3B, and 3C show an alternative mounting
16 configuration for the cymbal elements 10. FIG. 3A shows an
17 array of cymbal elements 10 in a partially cut away side view,
18 and FIG. 3B shows a top view of an array using this mounting.
19 In this embodiment, the cymbal elements 10 are held in place
20 around their outside rim with a rubber grommet 34 within a stiff
21 grid 36. Grommet 34 absorbs vibrations and prevents transfer of
22 these vibrations to grid 36 or between elements 10. Grommet 34
23 has an inner groove 38 receiving cymbal element 10 and an outer
24 groove 40 contacting grid 36.

1 The projector design taught in this invention allows for
2 great flexibility in electrical wiring configurations. For
3 instance, instead of electrically wiring in parallel such as in
4 the device described above, each cymbal element 10 or groups of
5 cymbal elements could be wired for individual addressing by
6 individual wires or other conductors 42 which combine to form a
7 wiring harness 44. The bottom side can be configured in a
8 similar fashion or it can use the conductive ribbons taught in
9 FIGS. 2C and 3C. This would allow for manipulation of electrical
10 impedance, control of beam forming capability through variation
11 of the radiating aperture, and multipurpose acoustic objectives
12 because of this ability to form different apertures within the
13 radiation profile. This means that this device design can have
14 specific apertures for specific frequency bands and specific
15 sonar operations within the same sonar wet-end packaging.
16 Accordingly, this invention provides a projector element and
17 array wherein the low frequency acoustic output from the
18 projector primarily comes from the low frequency resonance
19 associated with the flexure of the cymbal caps. This resonance
20 can be manipulated via mass loading the individual cymbal
21 elements by adding additional nuts and washers. As additional
22 nuts (i.e., mass) are added to each individual cymbal driver, the
23 projector resonance frequency is decreased with the caveat of
24 reduced acoustic source level due to the larger volume velocity
25 required as frequency is lowered.

1 This projector design is capable of wide frequency coverage
2 because the lowest resonance frequency is controlled by the
3 cymbal cap design, aperture, and mass loading conditions, whereas
4 the upper frequency is determined by the diameter of the
5 piezoelectric ceramic drive element. Consequently, within the
6 same transducer volume package, a sonar capable of low frequency,
7 weapons frequency, and imaging frequencies can be realized.
8 Further manipulation of the operating frequency band can be
9 achieved through the use of different size cymbal elements within
10 the projector.

11 This projector design is also conducive to the formation of
12 volumetric arrays. In volumetric arrays, two planes of
13 transducers are separated by a given distance (typically a
14 quarter wavelength) so that highly directional (cardioid)
15 radiation beam responses can be realized.

16 Projectors that utilize this design exhibit hydrostatic
17 pressure dependence at low frequencies. However, acoustic
18 pressure vessel data show that the device can be used up to
19 pressures of 2 MPa with little degradation in performance. In
20 addition, when the device is exposed to very high pressures
21 (e.g., 5.52 MPa) and then returned to a lower pressure (0.02
22 MPa), catastrophic failure was not experienced. For higher
23 frequency operation (i.e., above 20 kHz), where the radial mode
24 of the piezoelectric ceramic disk (-100 kHz in this device) is
25 the primary contributor to acoustic source generation,

1 hydrostatic pressure dependence is negligible. The utilization
2 of this design should result in higher hydrostatic pressure
3 tolerance at low frequency. This means that through proper
4 design engineering, this projector design should be usable for
5 all sonar applications.

1 Attorney Docket No. 84309

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3 LIGHTWEIGHT UNDERWATER ACOUSTIC PROJECTOR

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5 ABSTRACT OF THE DISCLOSURE

6 A compound electro-acoustic transducer for producing
7 acoustic signals has a plurality of elements. Each element has a
8 piezoelectric disk with electrically conductive plates fixed on
9 the top and bottom sides of the piezoelectric disk. A stud is
10 joined to an outer face of each plate. Conductors can be joined
11 to each stud. The elements can be assembled on a resilient
12 structure to form an array. Elements can be used in the array or
13 individually accessed.

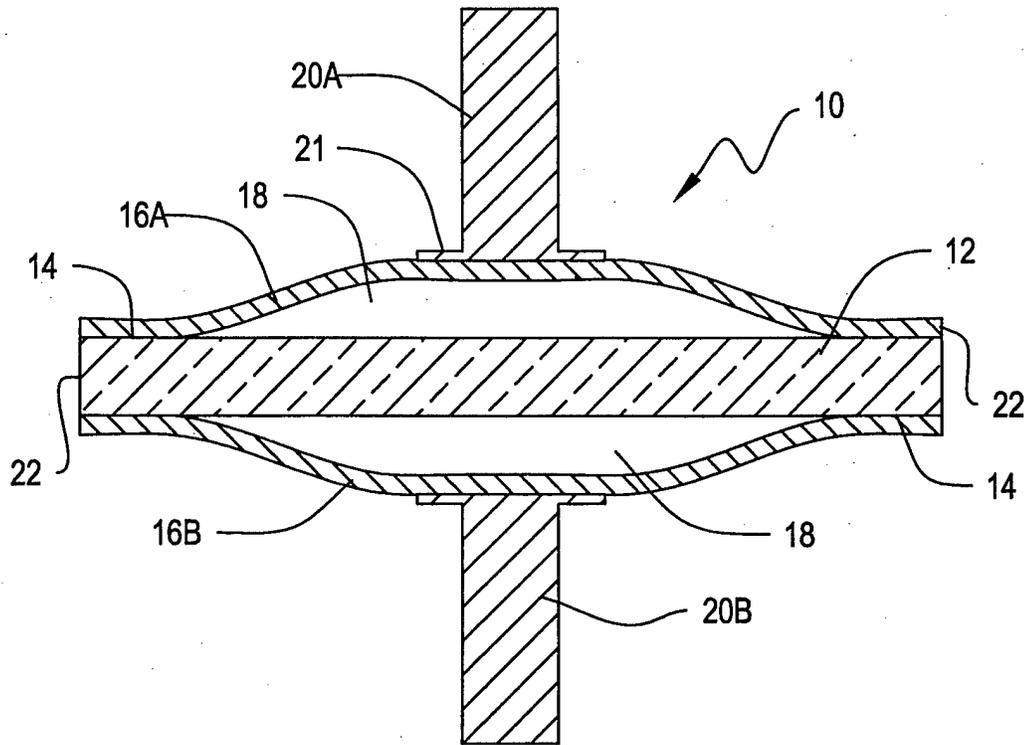


FIG. 1

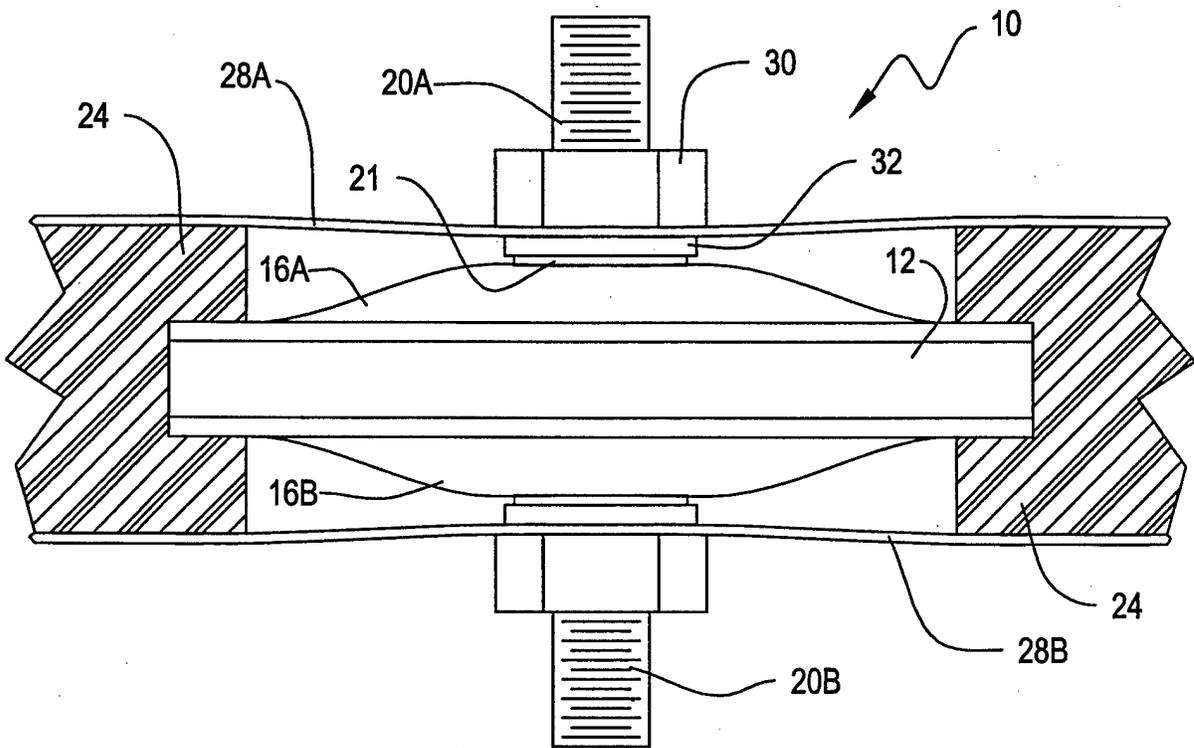


FIG. 2A

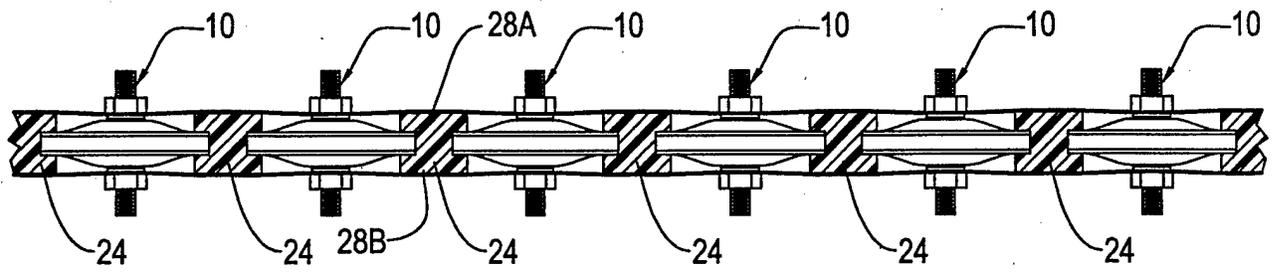


FIG. 2B

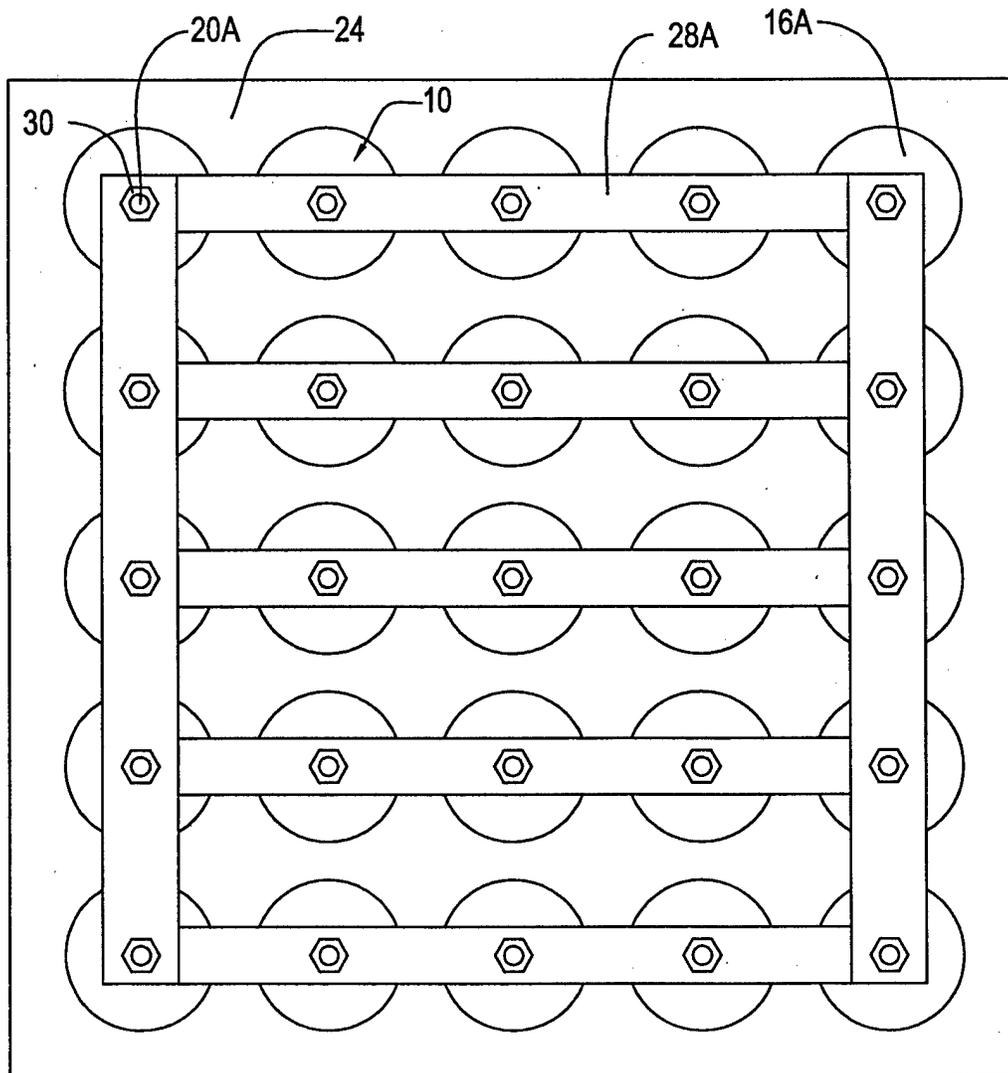


FIG. 2C

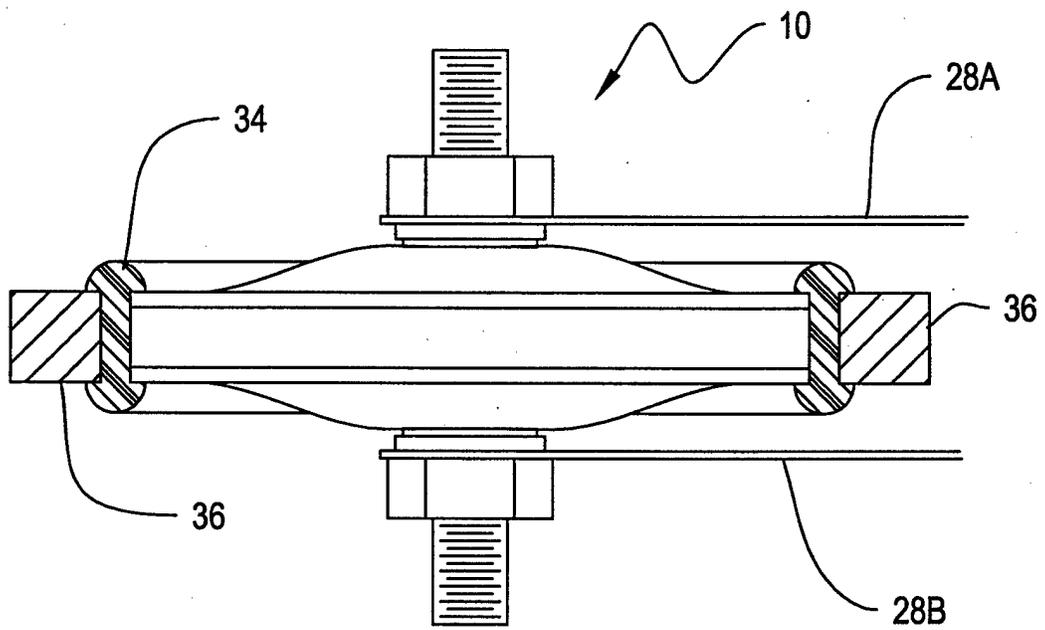


FIG. 3A

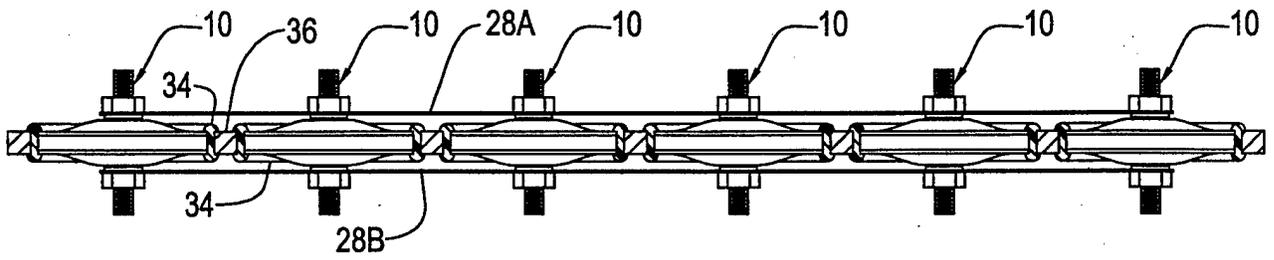


FIG. 3B

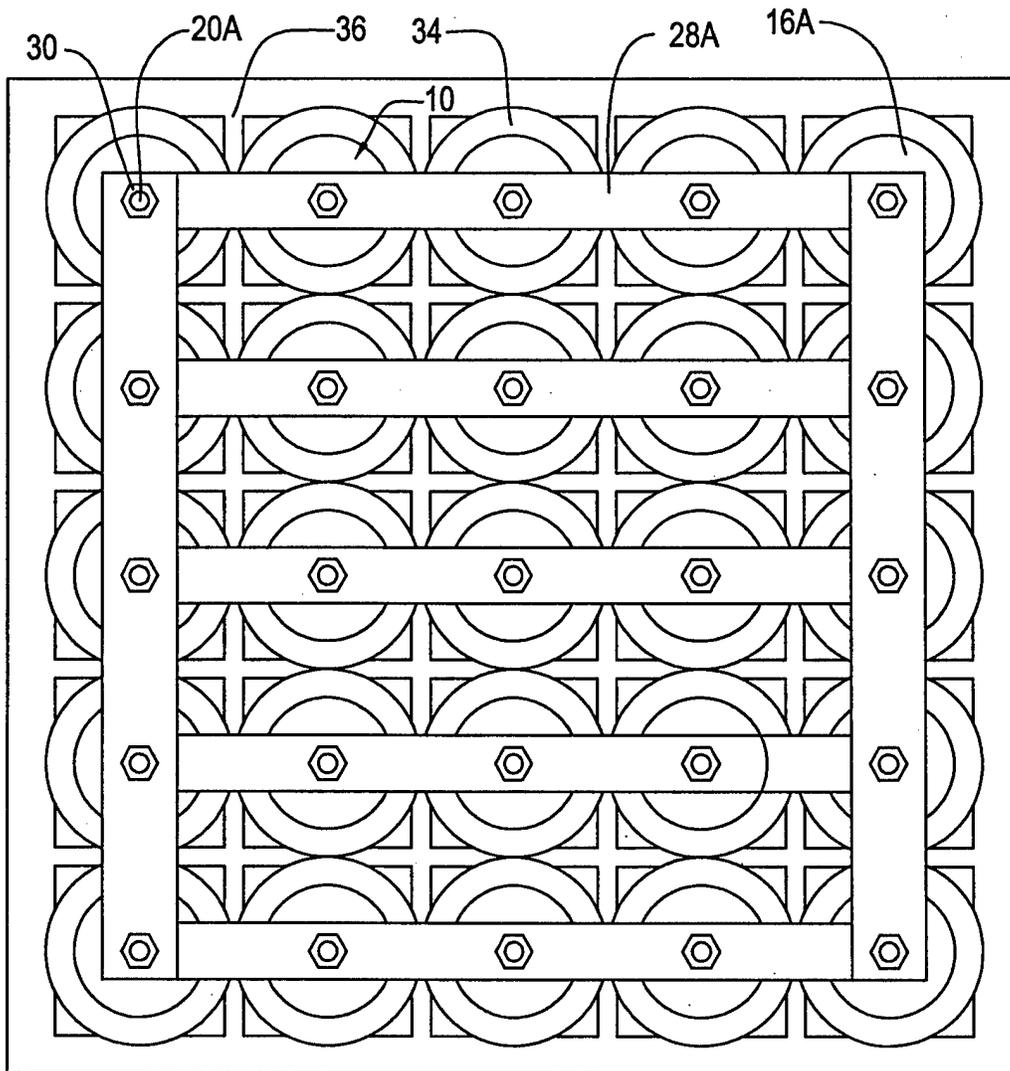


FIG. 3C

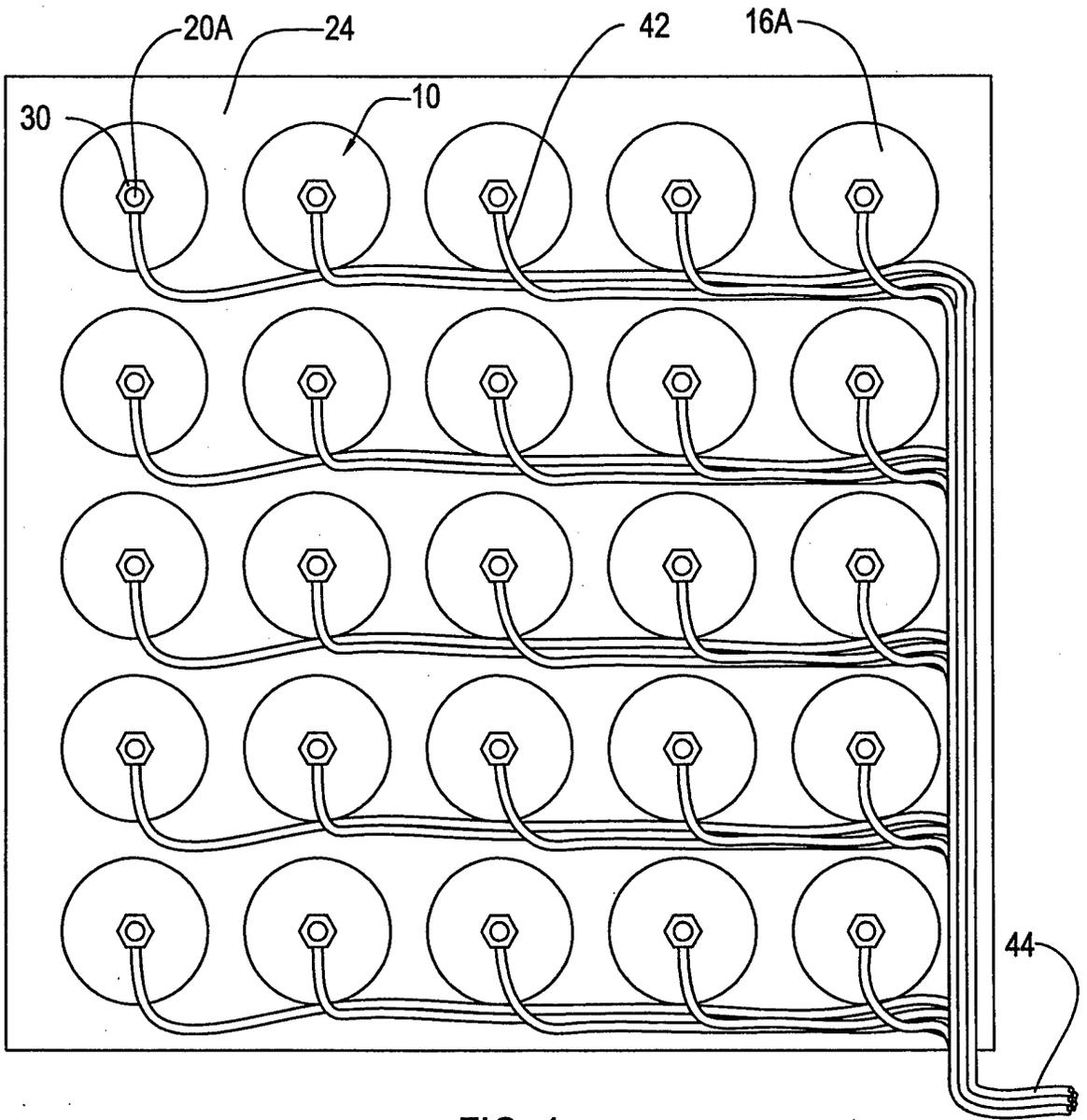


FIG. 4